

$$P(r) \sim \beta_s(r) \frac{\mathcal{P}(180,r)}{4\pi} exp(-2\beta \beta_e(r)dr)$$

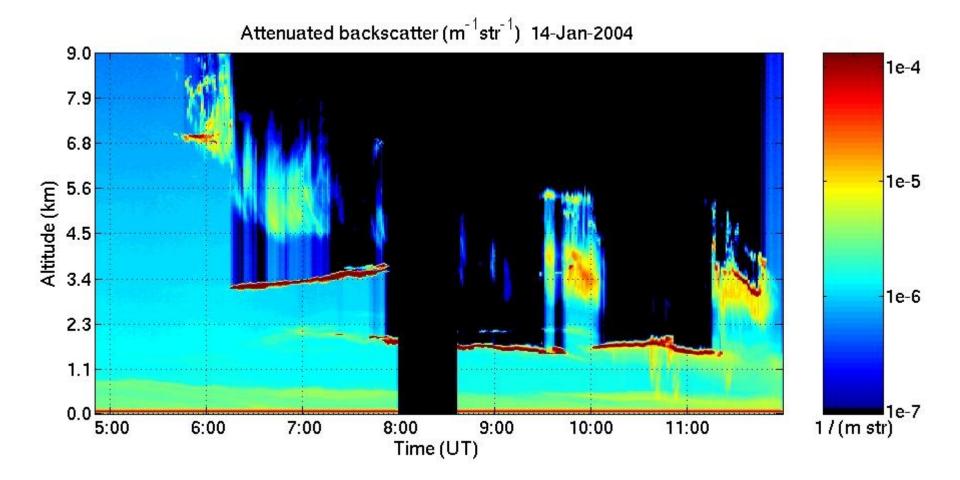
Traditional aerosol lidar can not distinguish between changes in target reflectivity and attenuation between the lidar and the target

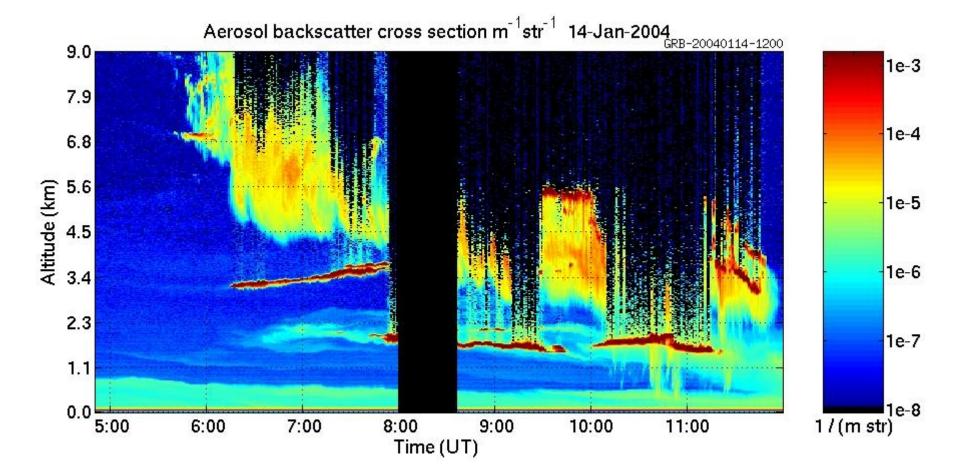
$$p_a(r) \sim \frac{1}{r^2} \cdot \frac{P(180,r)}{4\pi} \beta_a(r) \cdot exp(-2 \int (\beta_a(r) + \beta_m(r)) \cdot dr) - \text{aerosol return},$$

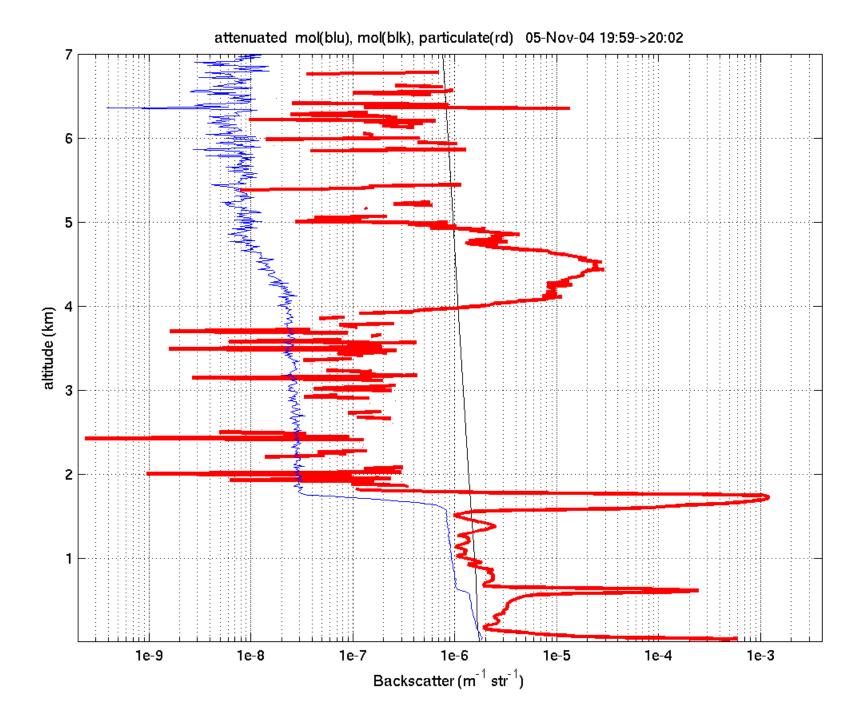
$$p_m(r) \sim \frac{1}{r^2} \cdot \frac{3}{8\pi} \beta_m(r) \cdot exp(-2 \int (\beta_a(r) + \beta_m(r)) \cdot dr) - \text{molecular return}$$

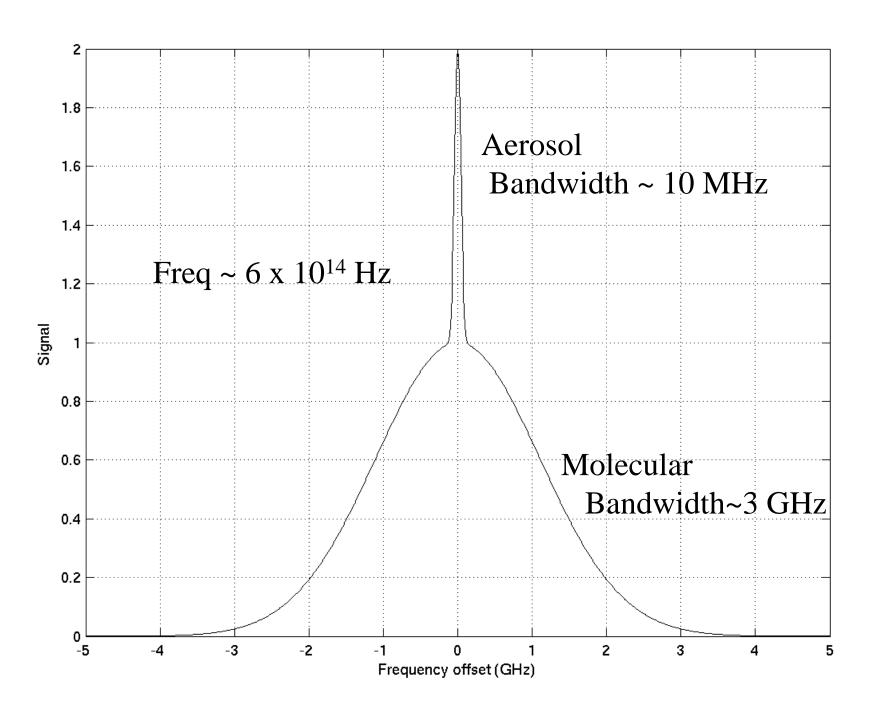
 $\beta'_a(r) = \frac{P(180,r)}{4\pi} \cdot \beta_a(r) = \frac{3}{8\pi} \cdot \beta_m(r) \cdot \frac{p_a(r)}{p_m(r)}$ The optical depth between r_1 and r_2 is derived by comparing the molecular return to that expected from a purely molecular atmosphere:

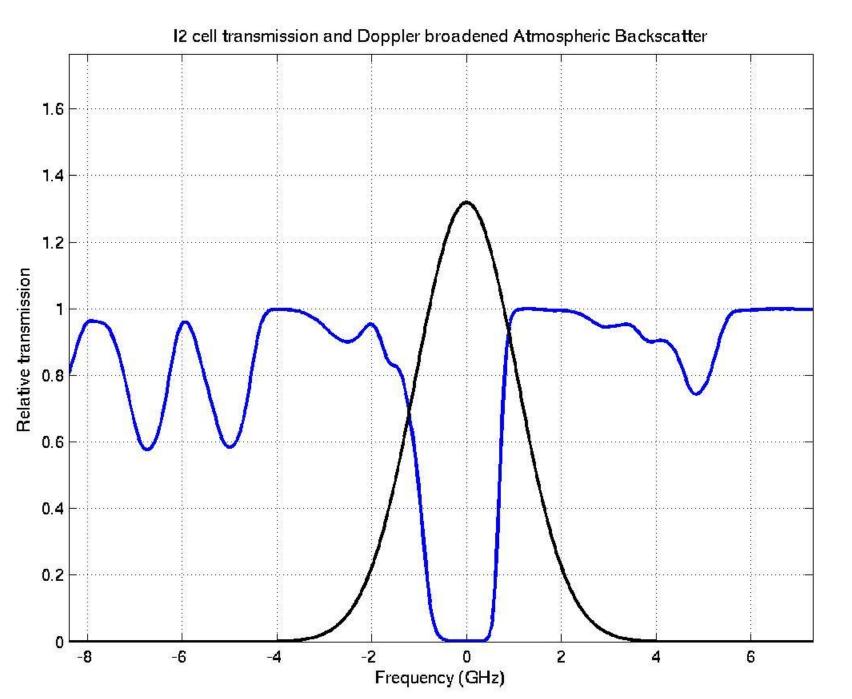
$$au(r_1,r_2) = rac{1}{2} \cdot log(rac{r_1^2
ho(r_2) \cdot p_m(r_1)}{r_2^2
ho(r_1) \cdot p_m(r_2)})$$

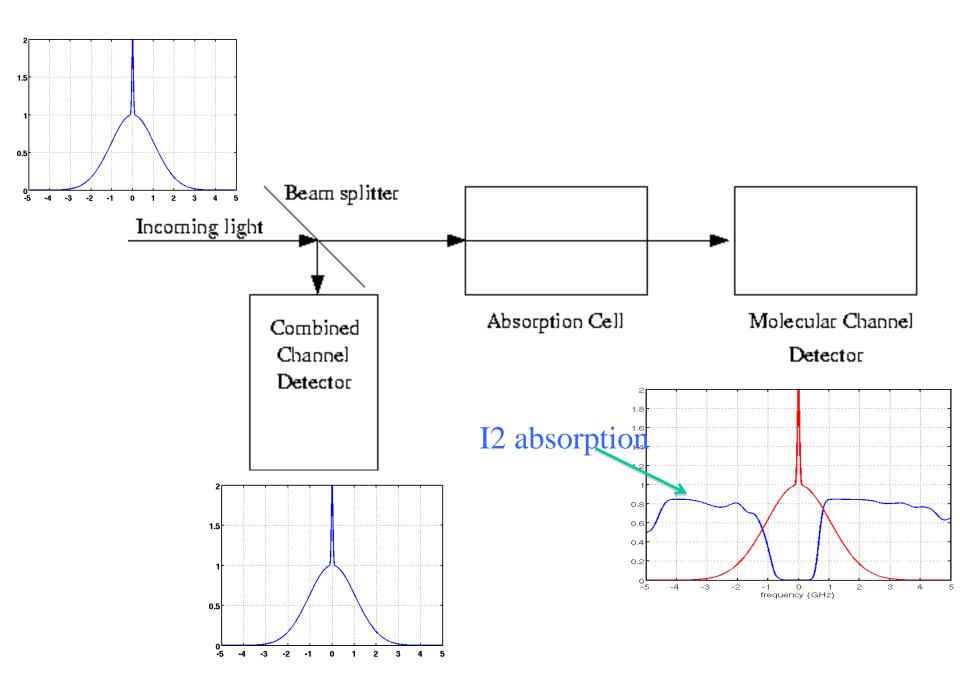


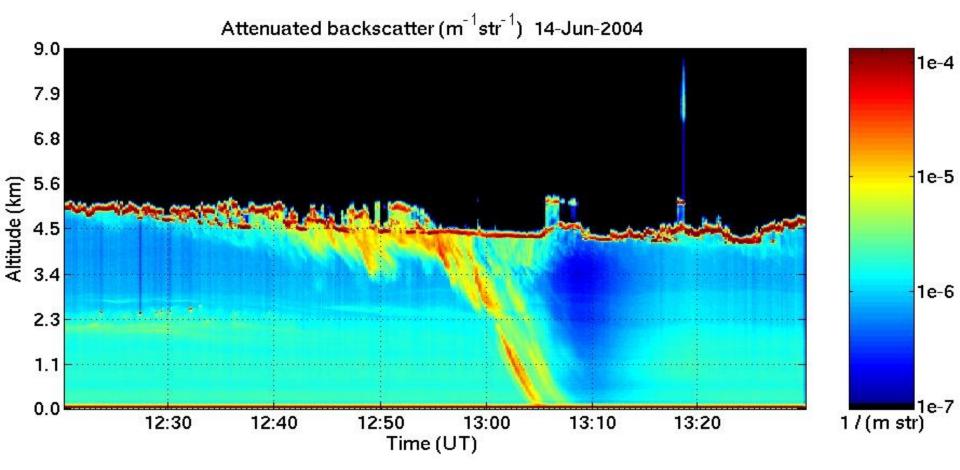


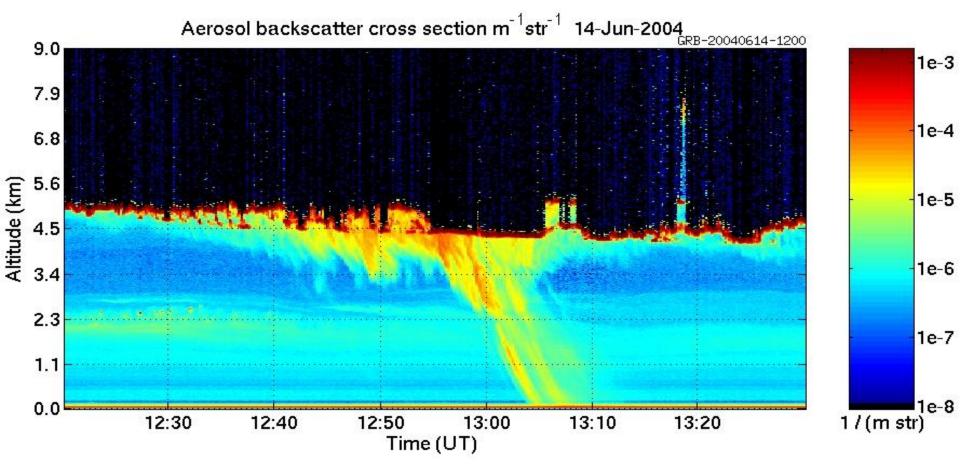




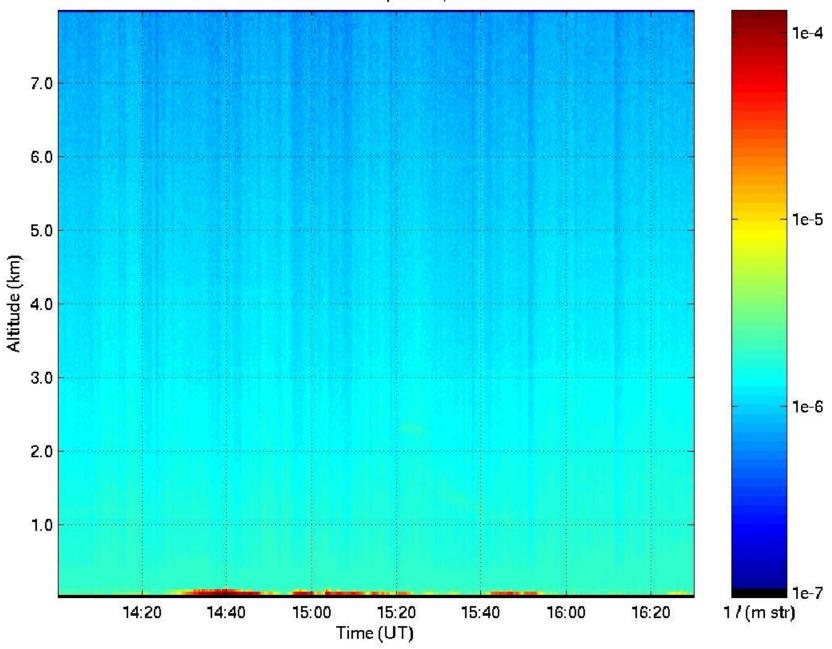


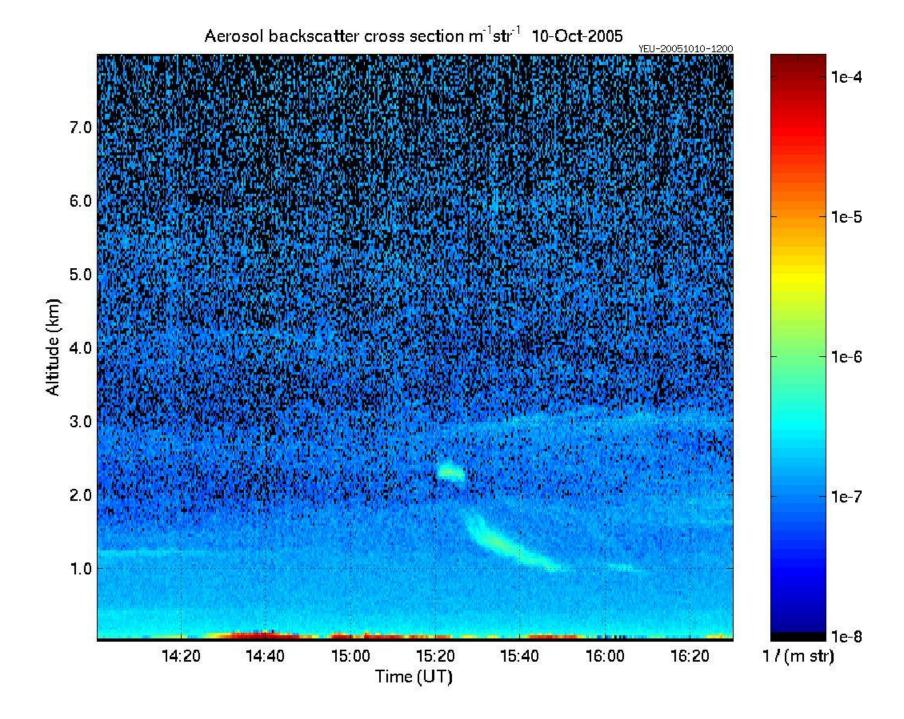


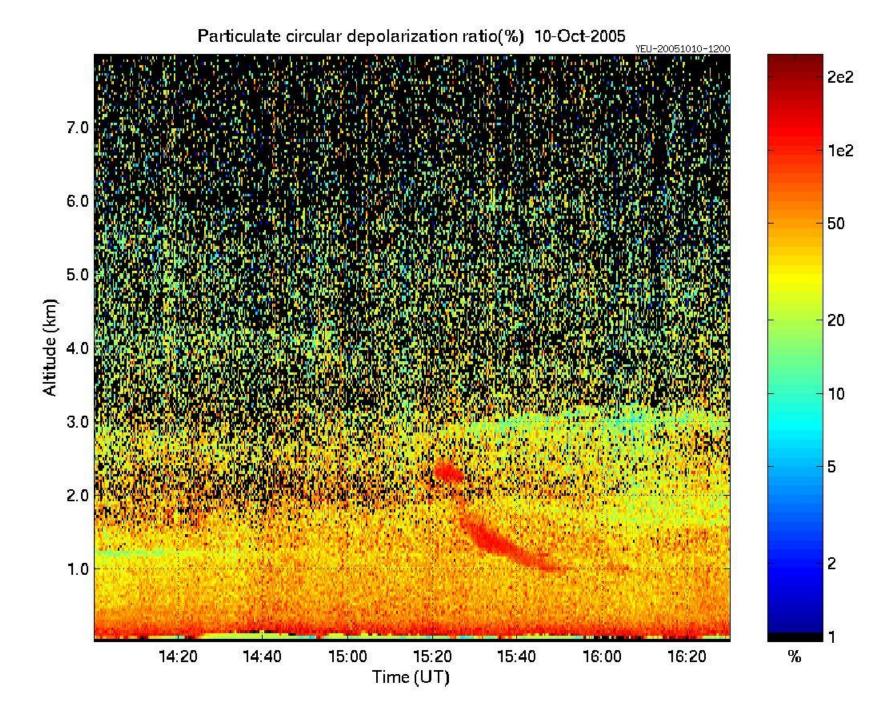


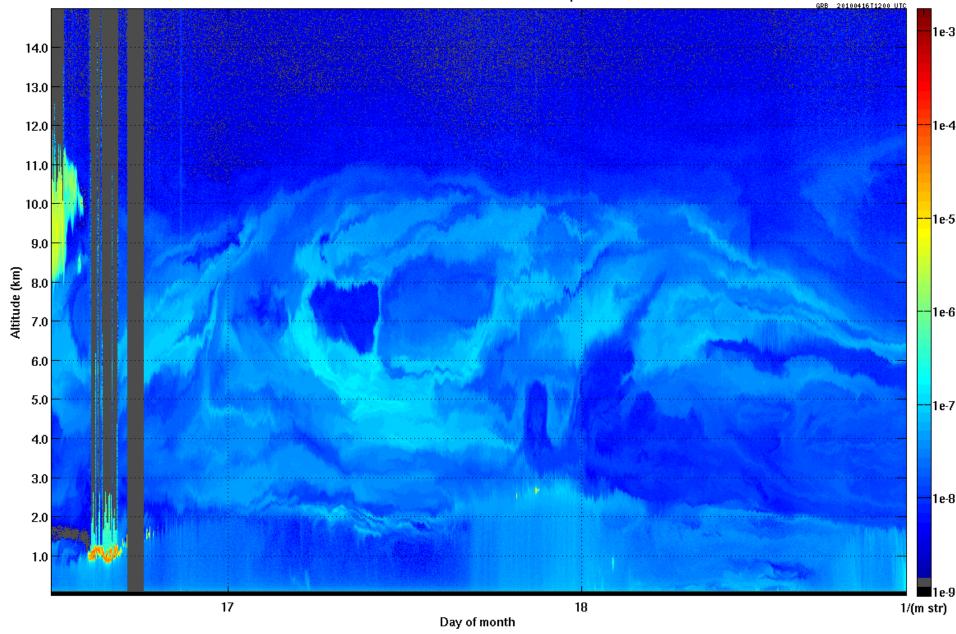


Attenuated backscatter (m⁻¹str⁻¹) 10-Oct-2005

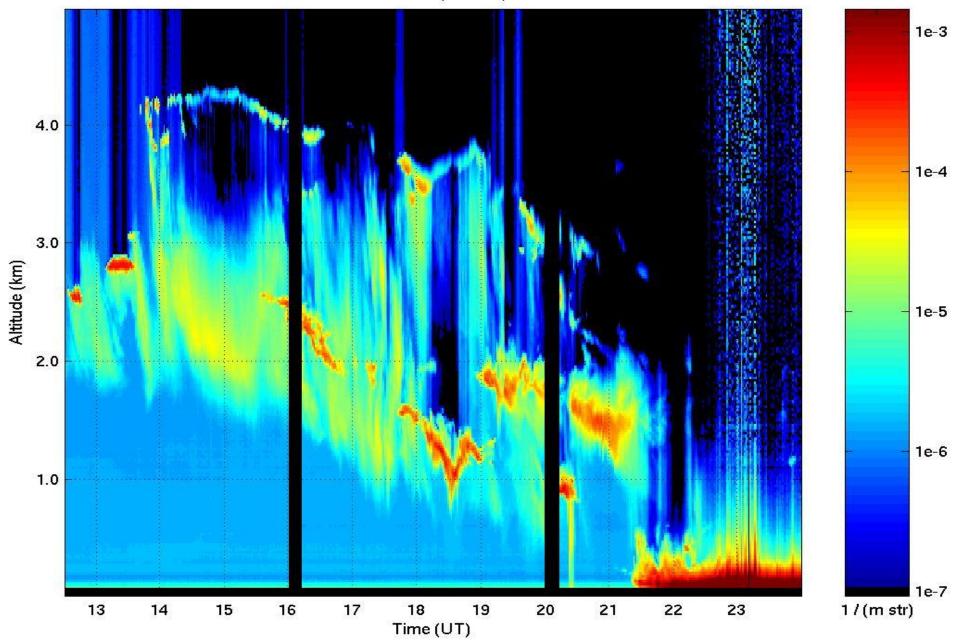




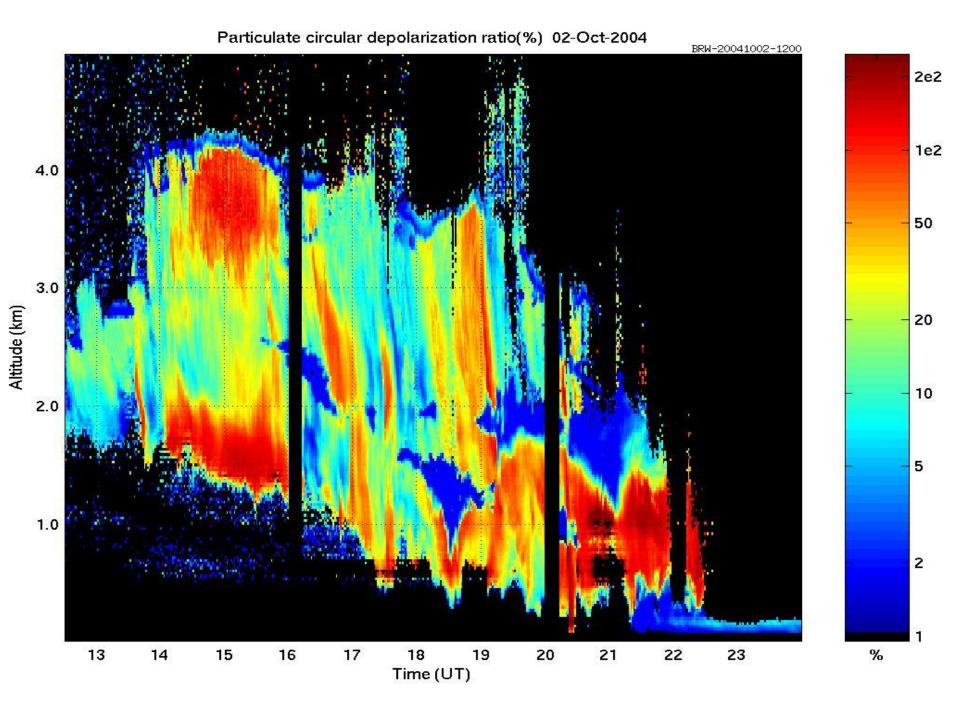


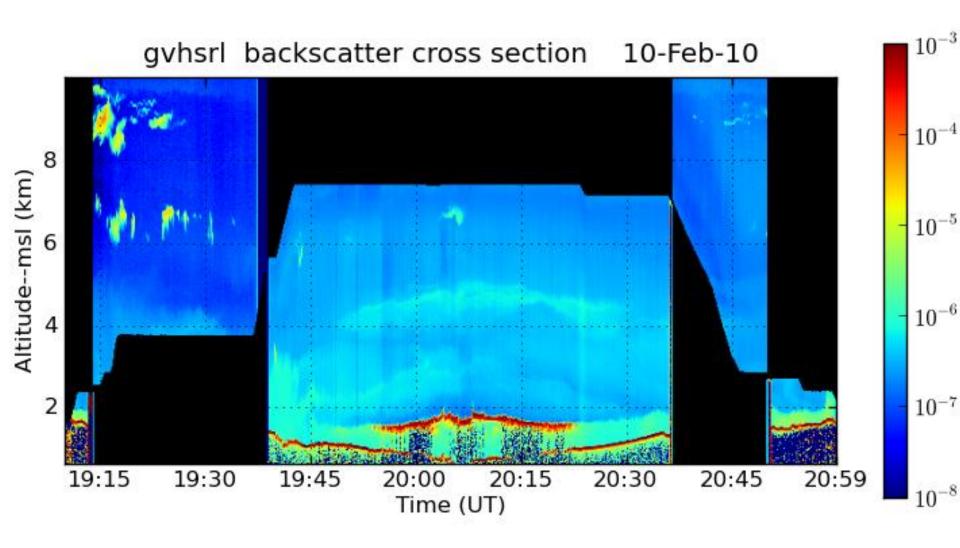


Attenuated backscatter (m⁻¹str⁻¹) 02-Oct-2004

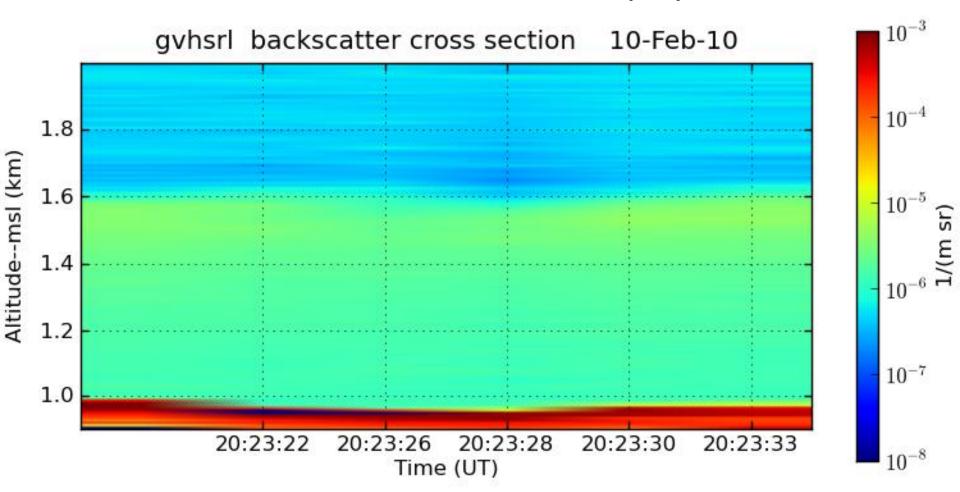


Aerosol backscatter cross section m⁻¹str⁻¹ 02-Oct-2004 BRW-20041002-1200 1e-3 4.0 1e-4 3.0 1e-5 Altitude (km) 2.0 1e-6 1.0 1e-7 1e-8 14 15 17 18 22 13 16 19 20 21 23 1 / (m str) Time (UT)

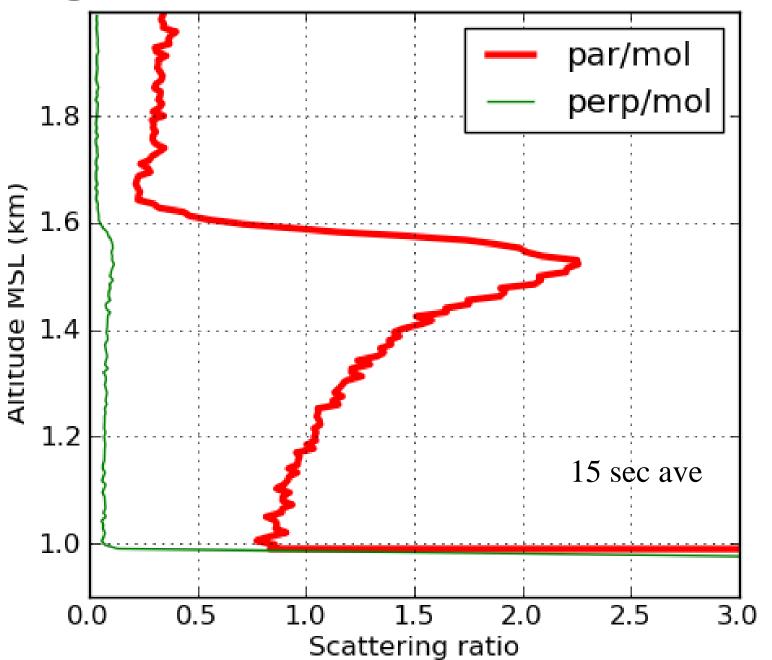




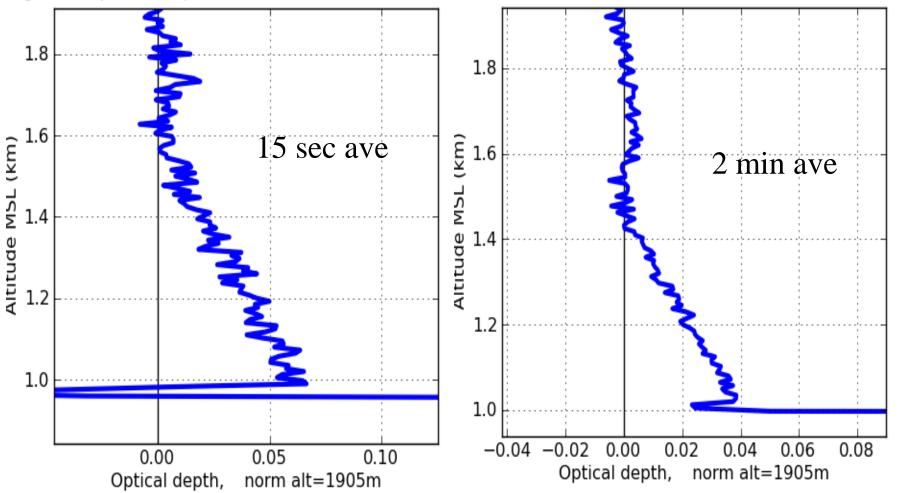
15-second observation of the boundary layer

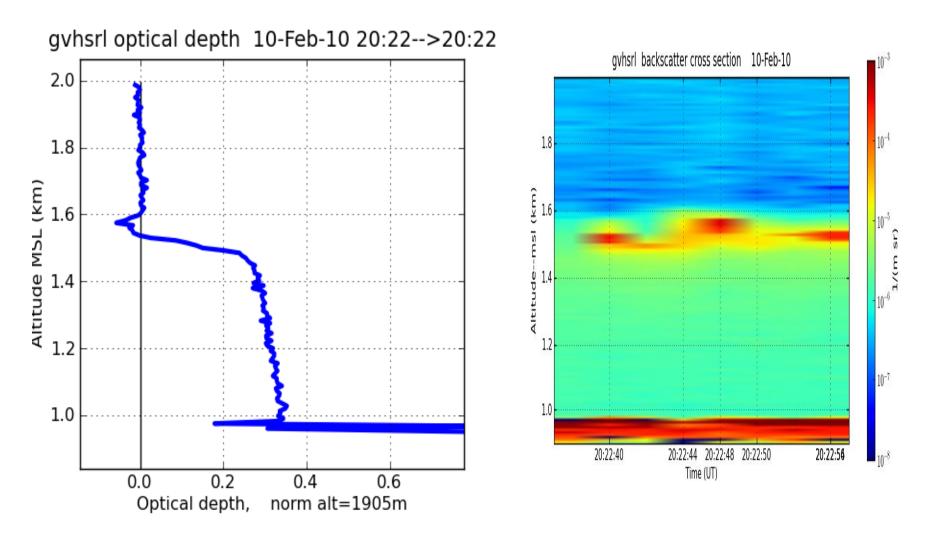


gvhsrl scat ratio 10-Feb-10 20:23-->20:23



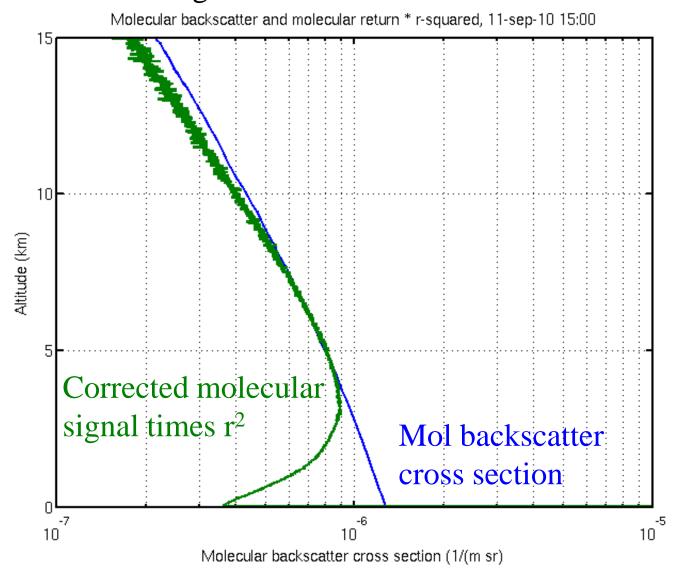
gvhsrl optical depth 10-Feb-10 20:23-->20:2 gvhsrl optical depth 10-Feb-10 20:23-->20:25

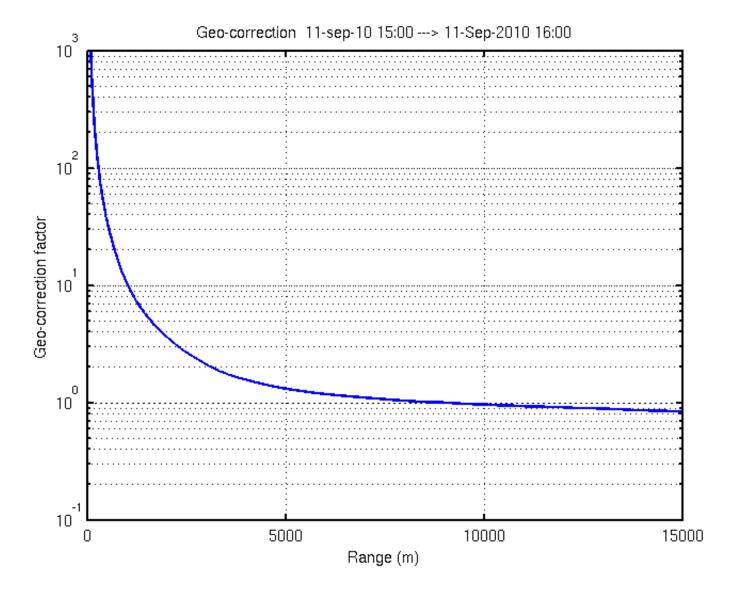


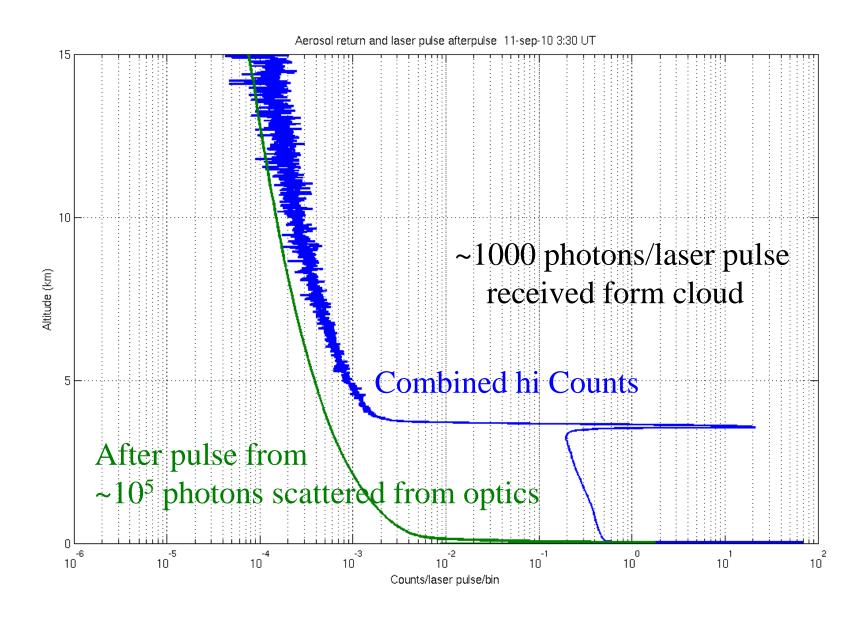


Optical depth profile for thin water cloud, 20 sec average

As the laser pulse propagates away from system the image size on the detector changes





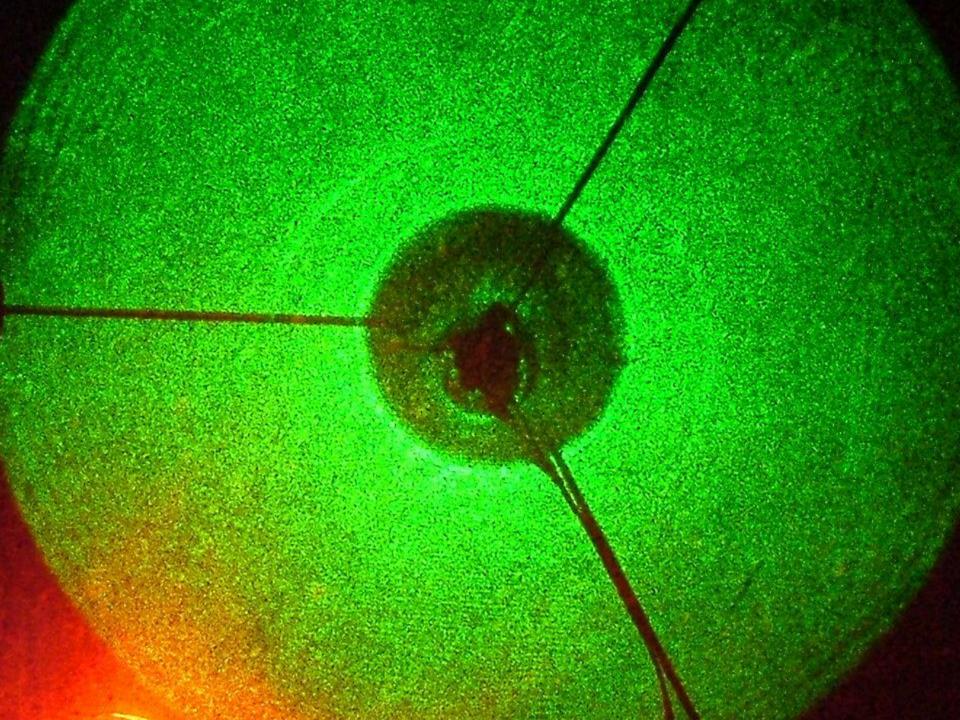


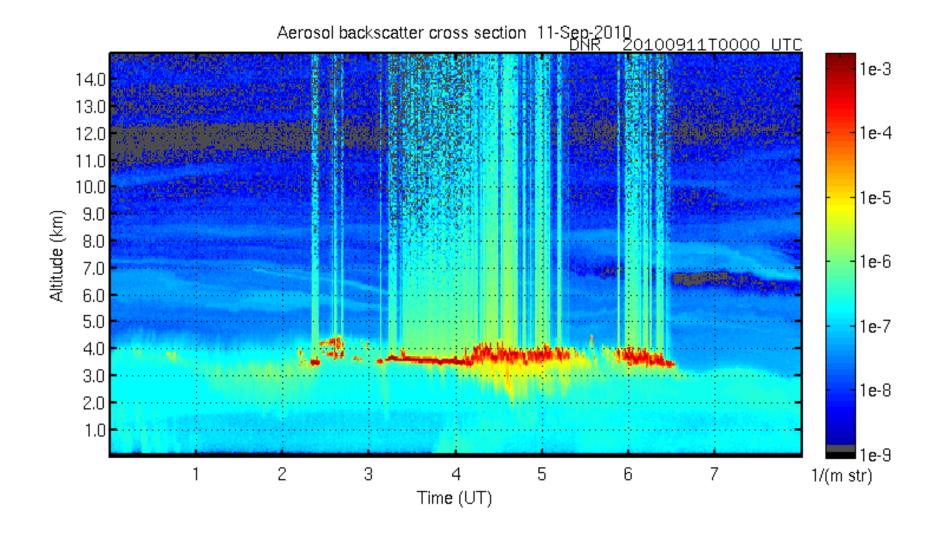
Advantages of 532 nm operation

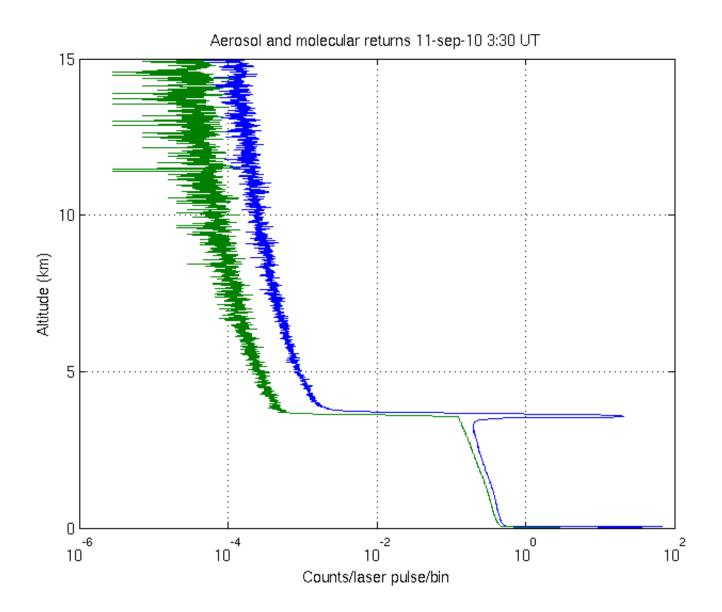
- -- Iodine adsorption line for filtering
- --Important wavelength for radiative transfer
- --Allows use of doubled Nd:YAG laser
- --Strong molecular scattering

Problem with 532 nm—eye safety

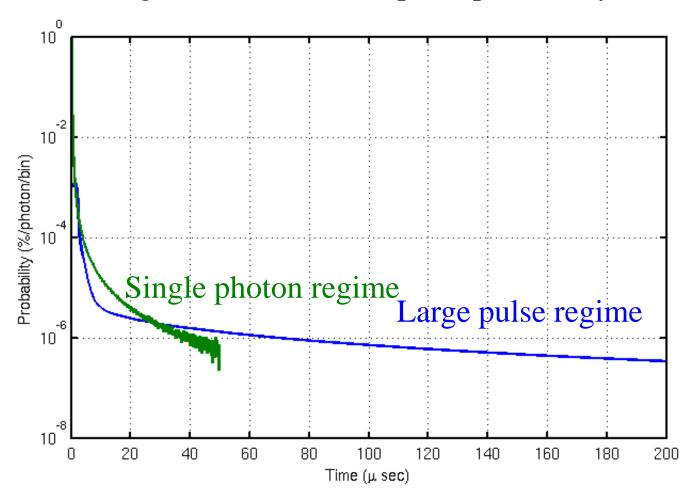
--Wavelength region with smallest permitted exposure max single pulse exposure = 5e-7 J/cm²

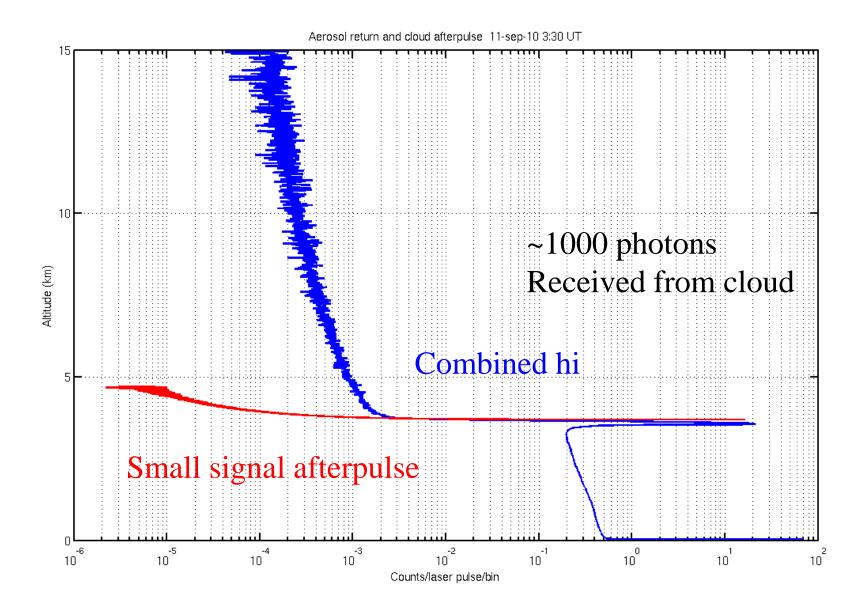


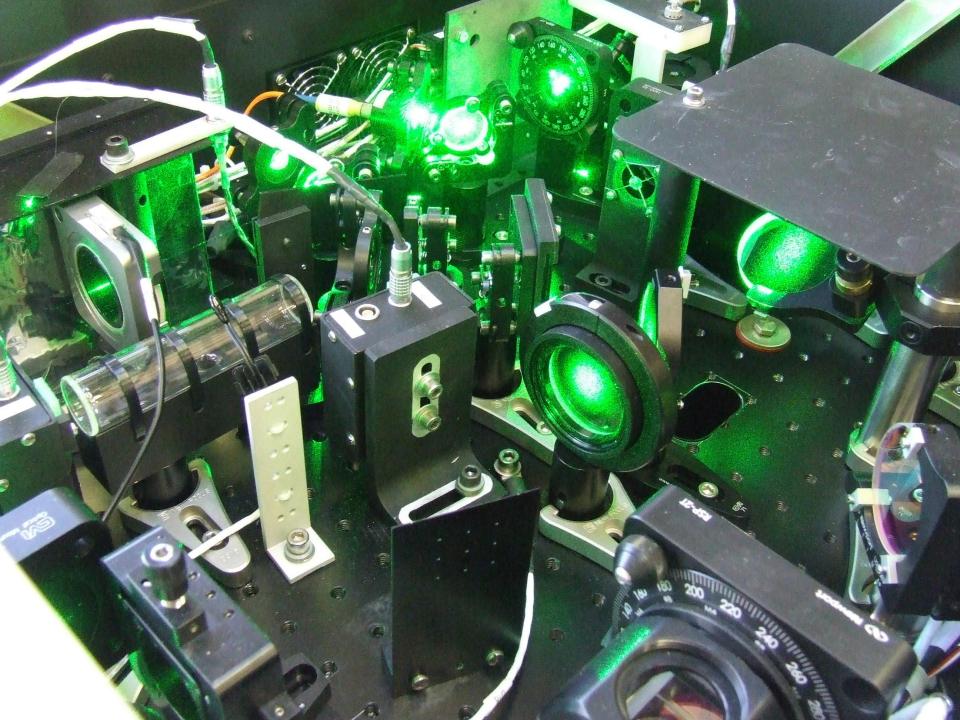


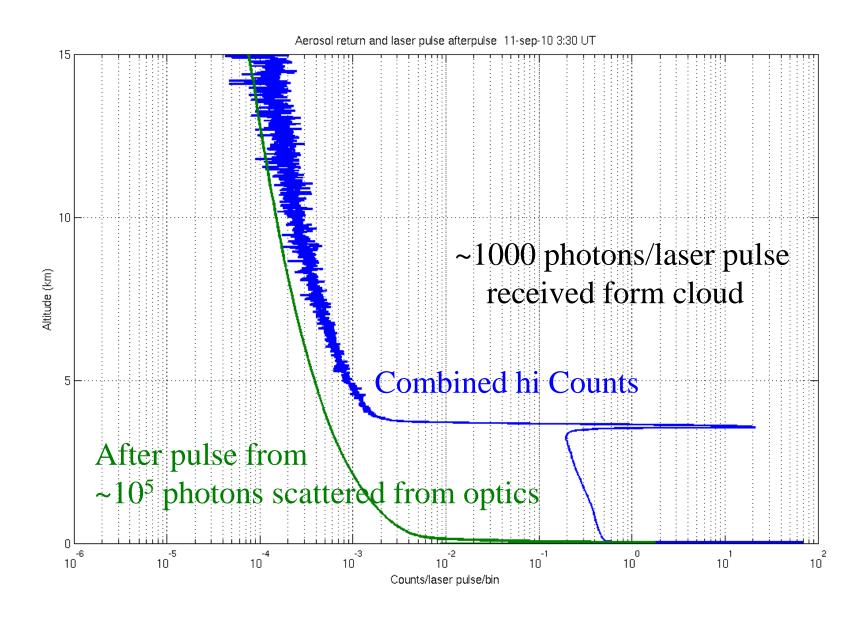


Geiger-mode APD afterpulse probability

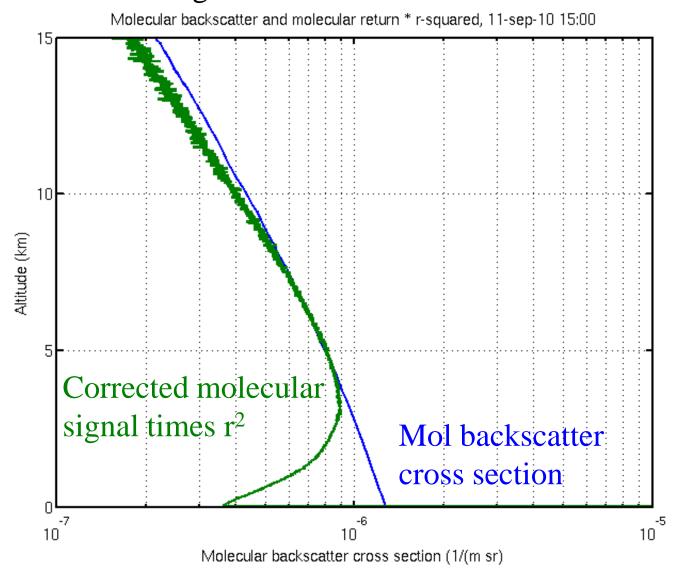


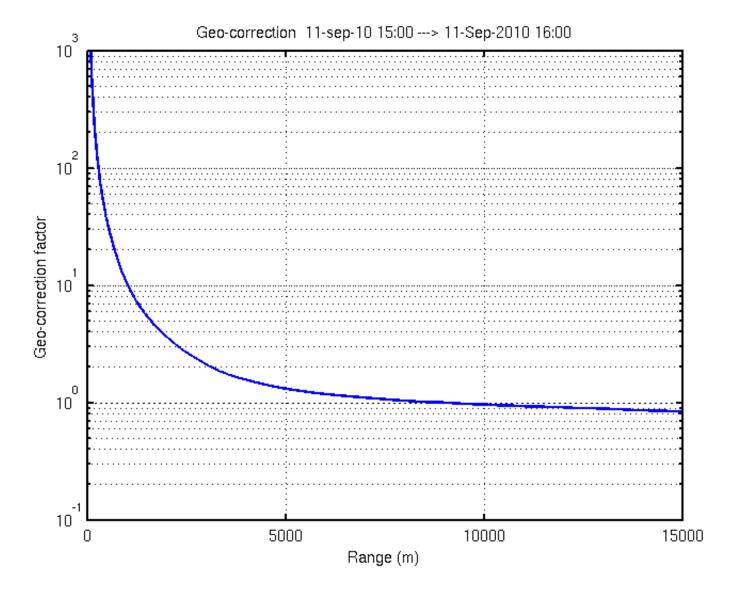


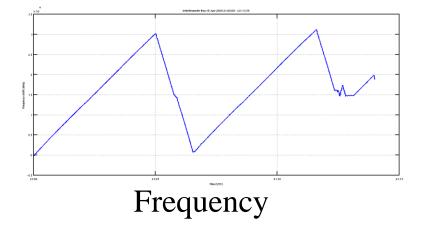




As the laser pulse propagates away from system the image size on the detector changes



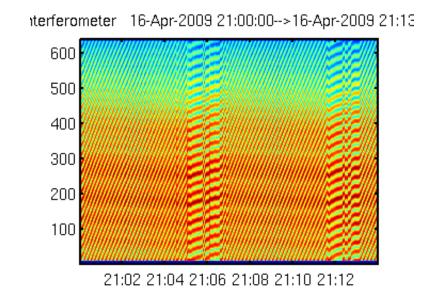




Molecular cal pulse 16-Apr-2009 21:00:00-->21:13:59 10 PUC Photons Photons/mJ Photons/laser pulse 21:00 21:00 21:05 21:10 21:15 time (UT)

The transmitter frequency is scanned over ~20 GHz to measure the spectral bandpass of the receiver

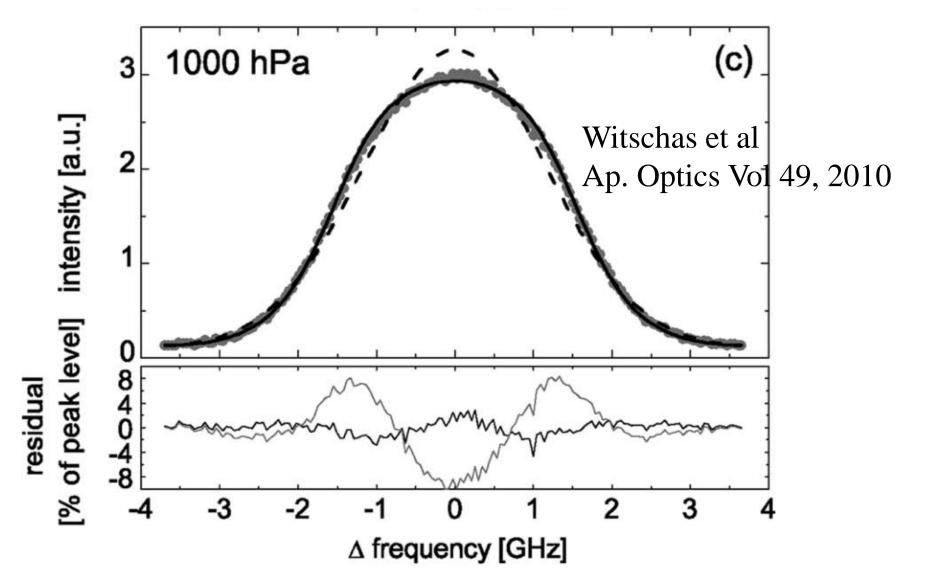
Receiver bandpass calibration



An interferometer is used to determine frequency during the spectral scan

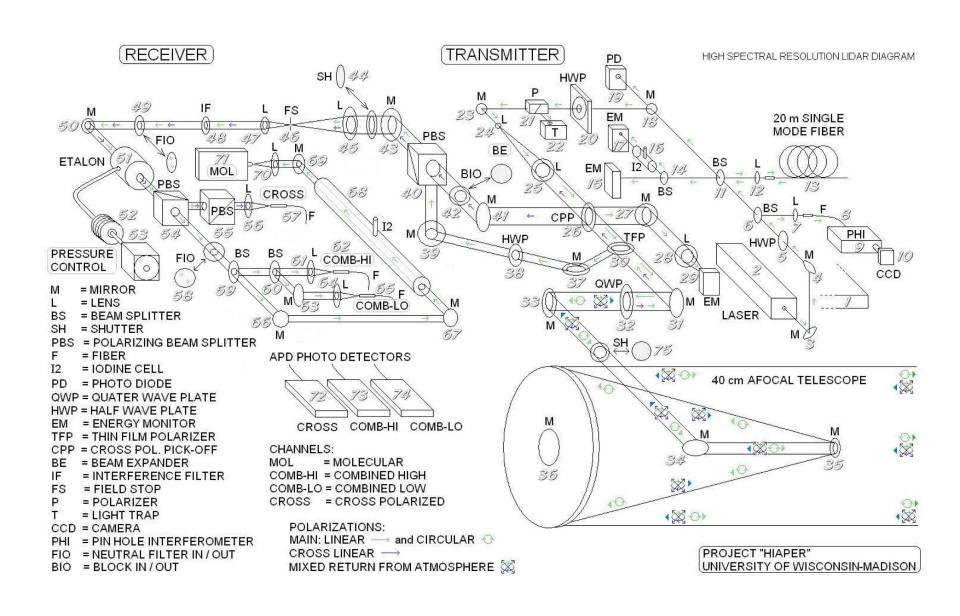
Completed Cal scan using interferometer freq ref 16-Apr-2009 20:59:00 10⁰ Relative transmission mol combined -3 **'** 10 12 measured smooth I2 measured 12 theory fit to comb -4 10 -10 -5 10

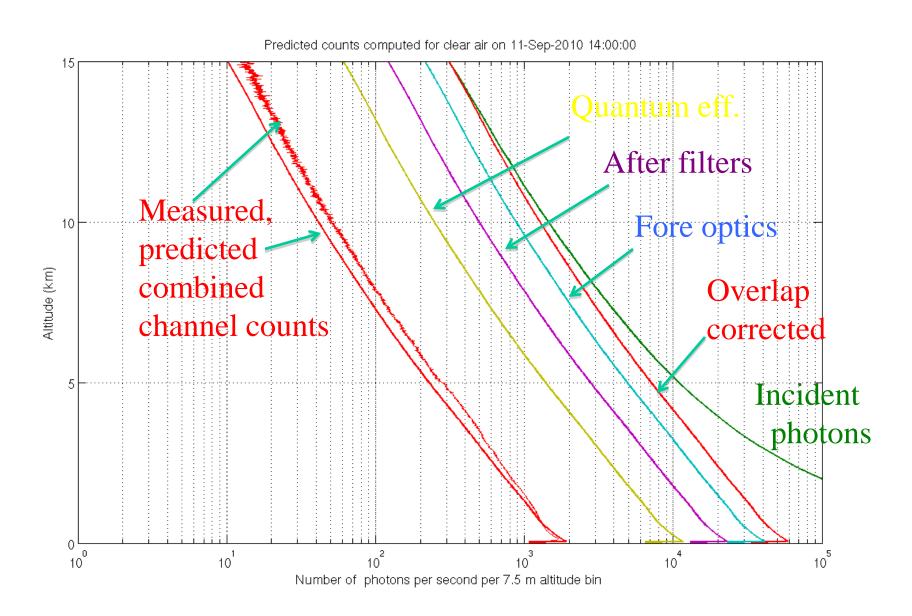
Frequency from interferometer (GHz)



Brillouin line shape at 1000 hPa (solid), Rayleigh line shape (dashed) and deviations from measured values using Tenti S6 and Rayleigh shapes

HSRL schematic – NCAR HAIPER version





Basic HSRL Equations

 $S_c = G_{ac}N_a + G_{mc}N_m$; eq 1—Signal in the combined channel

 $S_m = G_{am}N_a + G_{mm}N_m$; eq 2—Signal in the molecular channel

Where G_{ik} are gains of the two channels when exposed to N_a aerosol and N_m molecular photons.

Solving for N_m and N_a yields:

$$N_m = \frac{S_m/G_{am} - S_c/G_{ac}}{(G_{mm}/G_{am}) - (G_{mc}/G_{ac})}$$
; eq 3—Number of molecular photons incident as function of signals

$$N_a = \frac{S_c/G_{mc} - S_m/G_{mm}}{(G_{ac}/G_{mc}) - (G_{am}/G_{mm})}$$
; eq 4-Number of aerosol photons incident as function of signals

With G_{ac} =gain of the combined channel when exposed to aerosol photons

Define other gains relative to G_{ac} :

$$G_{mc} = C_{mc} \cdot G_{ac}, G_{am} = C_{am} \cdot G_{ac}, G_{mm} = C_{mm} \cdot G_{ac}$$

$$N_m = (1/G_{ac}) \cdot \frac{S_m/C_{am} - S_c}{(C_{mm}/C_{am}) - C_{mc}} = (1/G_{ac}) \cdot \frac{S_m - C_{am}S_c}{C_{mm} - C_{mc}C_{am}}$$

$$N_a = (1/G_{ac}) \cdot \frac{S_c/C_{mc} - S_m/C_{mm}}{(1/C_{mc}) - (C_{am}/C_{mm})} = (1/G_{ac}) \cdot \frac{S_c/C_{mc} - S_m/C_{mm}}{(1/C_{mc}) - (C_{am}/C_{mm})} = (1/G_{ac}) \cdot \frac{C_{mm}S_c - C_{mc}S_m}{C_{mm} - C_{mc}C_{am}}$$

The scattering ratio is then:

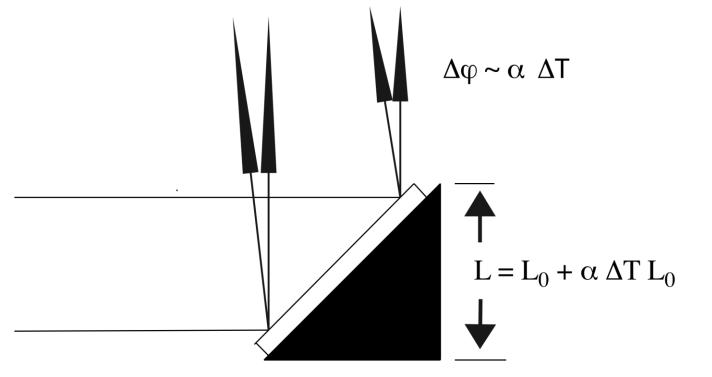
$$\frac{N_a}{N_m} = \frac{C_{mm}S_c - C_{mc}S_m}{S_m - C_{am}S_c}$$

The backscatter cross section, β'_a , is:

$$\beta_a'(r) = \beta_a(r) \cdot \frac{P(180,r)}{4\pi} = \frac{N_a(r)}{N_m(r)} \cdot \beta_m(r)$$
, where β_a =scattering cross section, $\frac{P(180,r)}{4\pi}$ =backscatter phase function.

the optical depth, τ , between two points $r_1 and r_2$ is:

$$\tau(r_2-r_1)=\frac{1}{2}\cdot log(\frac{r_1^2\rho(r_2)\cdot N_m(r_1)}{r_2^2\rho(r_1)\cdot N_m(r_2)})$$
, where $\rho(r)=$ the atmospheric density profile



Thermal expansion of components effect the alignment of transmitter with the receiver. Here we consider the example of an 45 deg aluminum mountin block for a beam turning mirror.

Angle shift due to 10 deg C temperature change: $\Delta \phi \sim \alpha \Delta T \sim 2.5 *10^{-5} * 10 \Delta \phi \sim 250$ microradian

Problem with 532 nm—eye safety

--Wavelength region with smallest permitted exposure

ANSI safe exposure \leq 5e-7 (R/4)-1/4 J/cm²

Where R = the pulse repetition rate

This forces high repetition rate and large apertures

Range ambiguity limits R < \sim 4kHz, i.e. r_{max} < \sim 40 km

Cost, complexity, turbulence limit aperture to ~0.5 m.

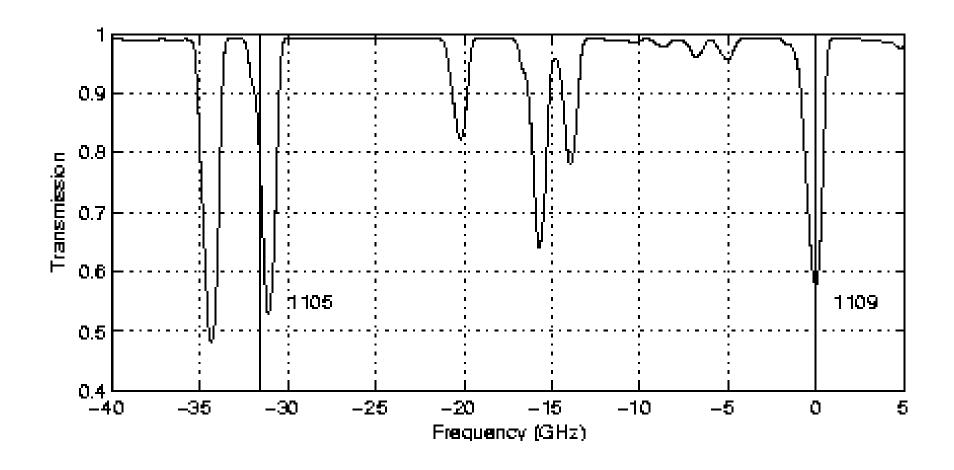
Thus max transmitted energy laser pulse is limited to:

 $\pi 25^{2*}5e-7*1000^{-1/4}=0.174 \text{ mJ/pulse}$

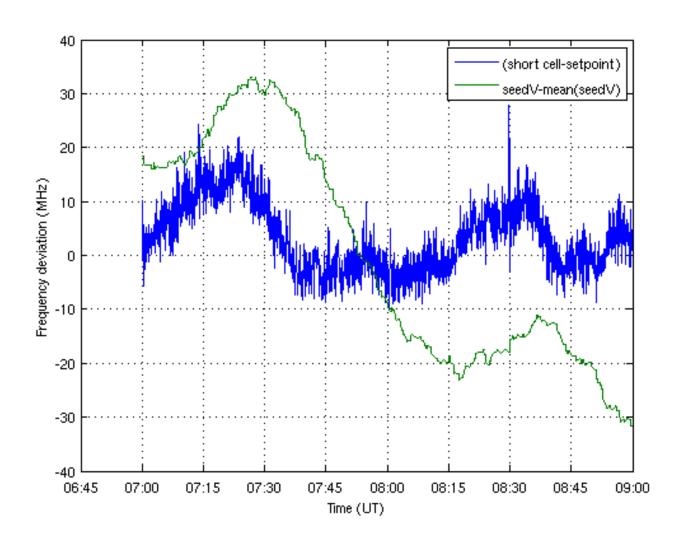
and the maximum transmitted power is:

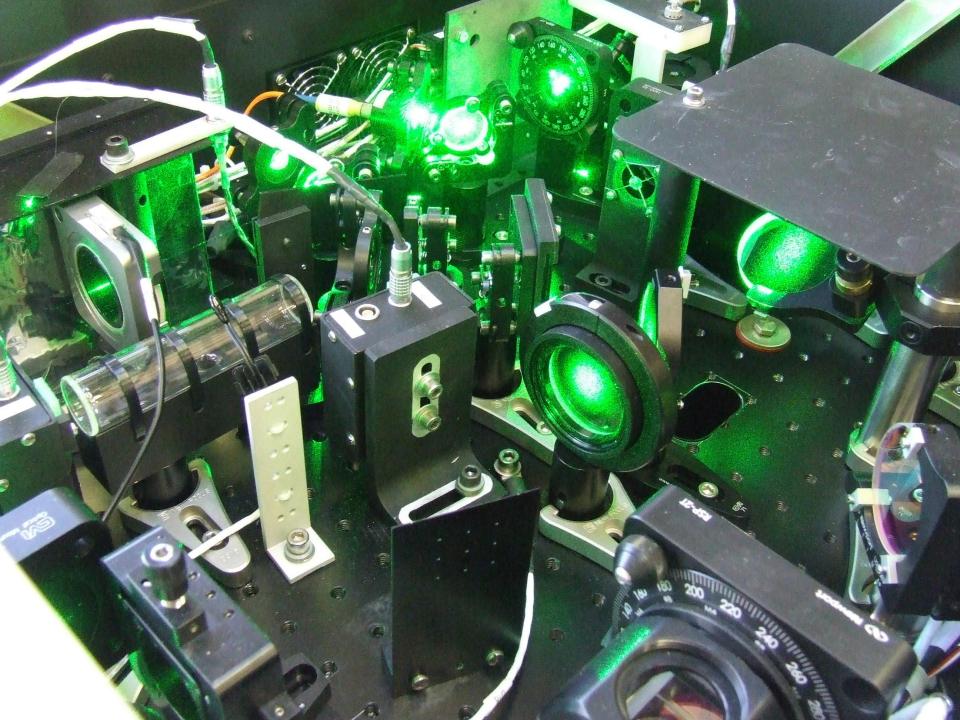
0.174e-3*4000 Hz = 0.7 Watt

Transmission of 2-cm iodine cell



Example of frequency locking





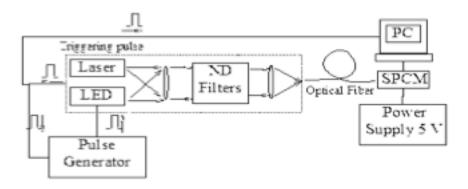
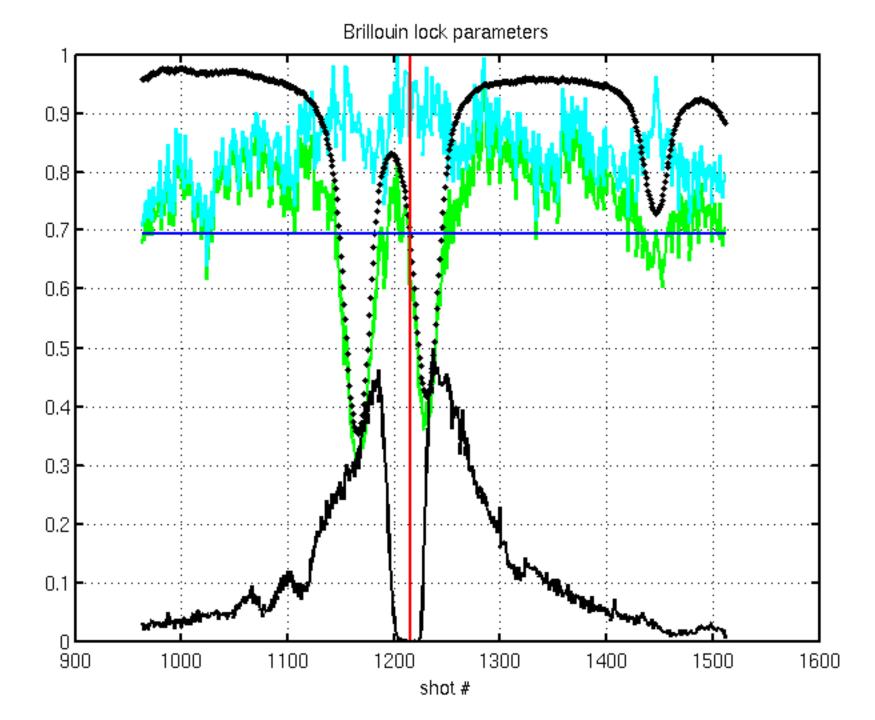
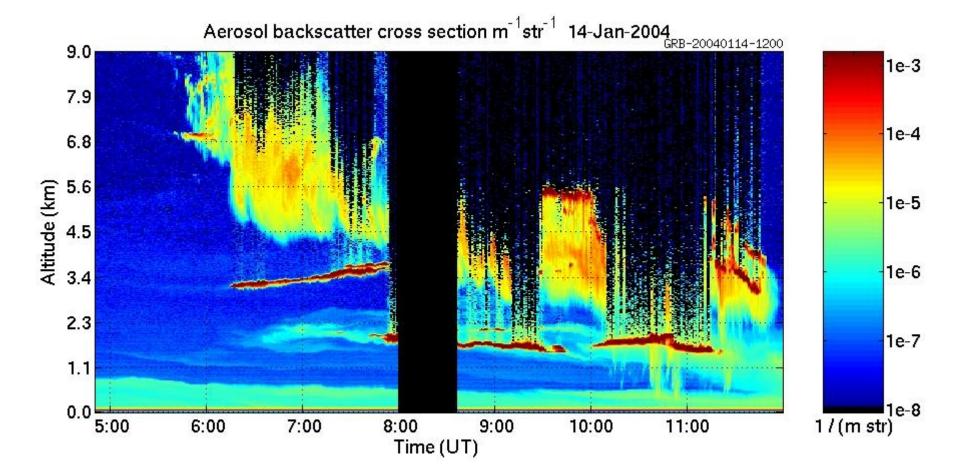


Figure 4. A block-diagram of the experimental setup.

2.2 Detector impulse response function







Specifications

Transmitter:	GVHSRL	Langley HSRL

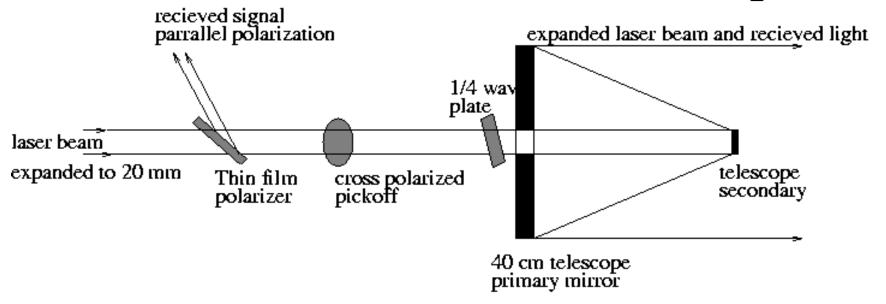
Repetition rate	4000 Hz	200 Hz
Wavelength	532 nm	532 nm
Energy	82 uJ	2.5 mJ
Ave power	339 mW	500 mW

Receiver:

Aperture	40 cm	40 cm
Bandwidth	8 GHz	60 GHz
Quantum Eff	55%	10% (?)
Field of View	100 μrad	250-1000 μrad
Optical trans	~34%	57%

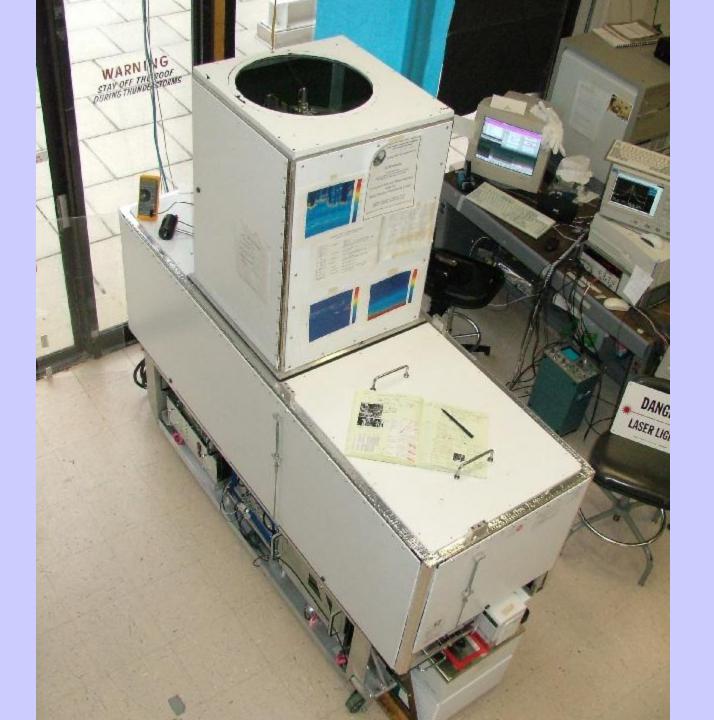
Signal strength ~ 1 0.27 (Area*Pwr*QE* η) Sky Noise ~ 0.24 3.4 (Area*BW* Ω *QE* η)

AHSRL transmit-receive telescope



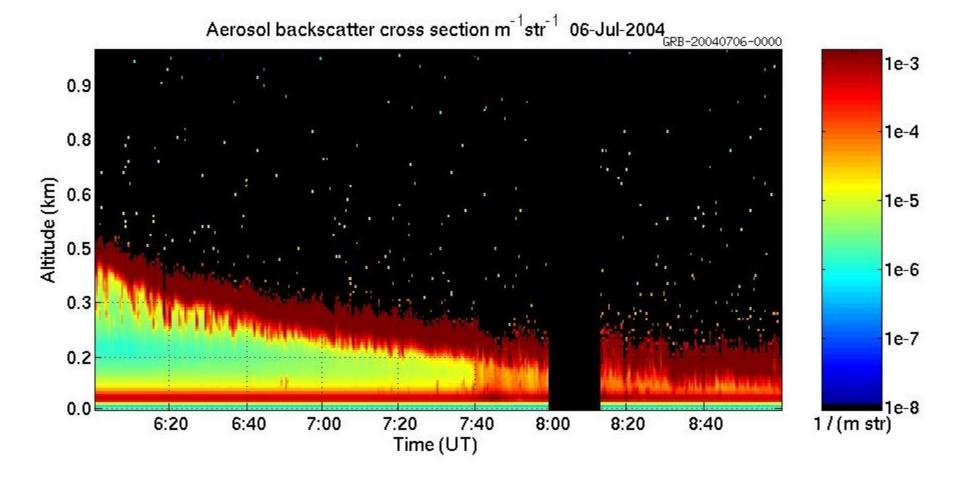
- -- The 20 mm diameter linearly-polarized laser beam is converted to circular polarization by ¼ wave plate before expansion 40 cm.
- --The received signal is converted to linear polarization on return through the ¼ wave plate. Approx. 10% of the signal is separated to measure the cross-polarized component. The parallel-polarized component is separated from the transmit beam by the thin-film polarizer.

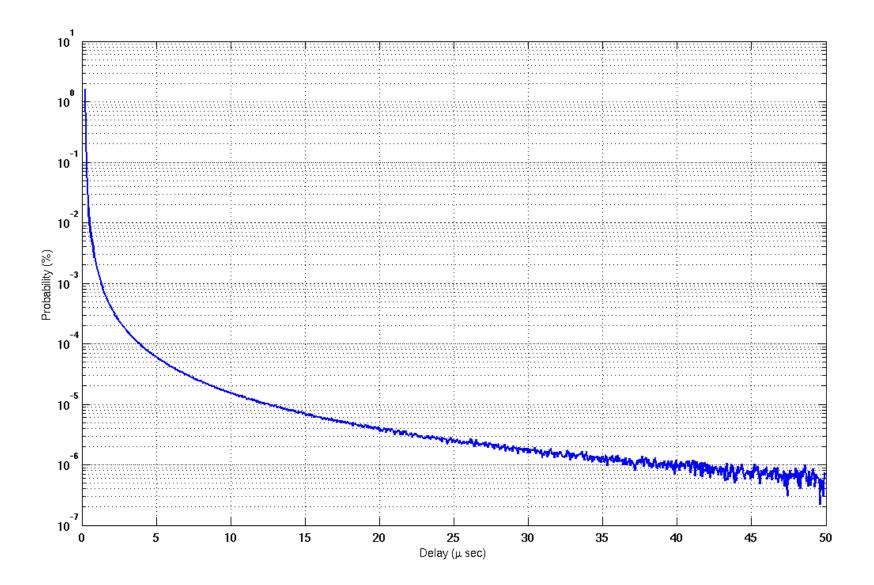




High Spectral Resolution Lidar at North Slope ARM site







Arctic HSRL Specifications

• Altitude coverage ~75m-->30 km

• Altitude resolution 7.5 m

• Time resolution :

• Backscatter, depolarization profiles 0.5 sec

• -Optical depth profiles >20 sec

• Eye safe at output

• Wavelength 532 nm

• Power $200 \rightarrow 600 \text{ mW}$

• Repetition rate 4 kHz

• Field of view 45 microradians

• Sky noise filter bandwidth 8 GHz

• Typical background noise/bin >1 photon/1000 laser pulses

• Receiver diameter 0.4 m

• I2 filter bandwidth 1.8 GHz

